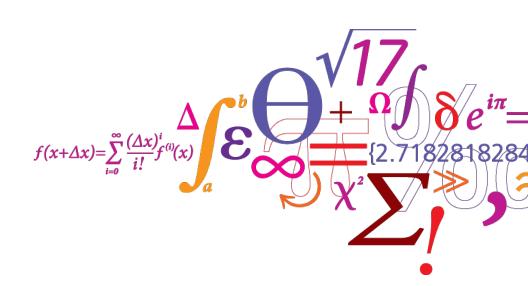
31730: Electric Power Engineering, fundamentals

DTU

Transmission Lines

Spyros Chatzivasileiadis

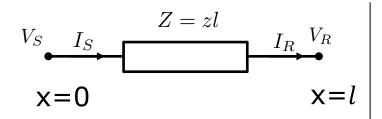


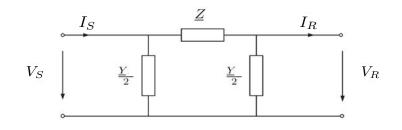


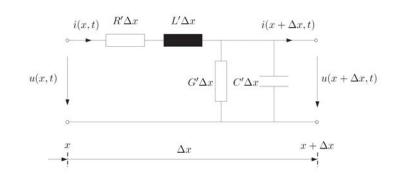
DTU Electrical EngineeringDepartment of Electrical Engineering



Line Models



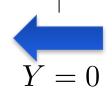




$$\begin{bmatrix} V_S \\ I_S \end{bmatrix} = \begin{bmatrix} 1 & Z \\ 0 & 1 \end{bmatrix} \begin{bmatrix} V_R \\ I_R \end{bmatrix}$$

$$\begin{bmatrix} V_S \\ I_S \end{bmatrix} = \begin{bmatrix} 1 & Z \\ 0 & 1 \end{bmatrix} \begin{bmatrix} V_R \\ I_R \end{bmatrix} \qquad \begin{bmatrix} V_S \\ I_S \end{bmatrix} = \begin{bmatrix} 1 + \frac{YZ}{2} & Z \\ Y\left(1 + \frac{YZ}{4}\right) & 1 + \frac{YZ}{2} \end{bmatrix} \begin{bmatrix} V_R \\ I_R \end{bmatrix} \qquad \begin{bmatrix} V_S \\ I_S \end{bmatrix} = \begin{bmatrix} \cosh(\gamma l) & Z_c \sinh(\gamma l) \\ \frac{1}{Z_c} \sinh(\gamma l) & \cosh(\gamma l) \end{bmatrix} \begin{bmatrix} V_R \\ I_R \end{bmatrix}$$

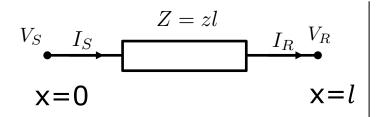
$$\begin{bmatrix} V_S \\ I_S \end{bmatrix} = \begin{bmatrix} \cosh(\gamma l) & Z_c \sinh(\gamma l) \\ \frac{1}{Z_c} \sinh(\gamma l) & \cosh(\gamma l) \end{bmatrix} \begin{bmatrix} V_R \\ I_R \end{bmatrix}$$



$$\gamma l << 1$$

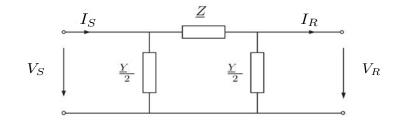


Line Models



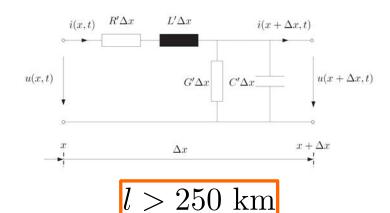
$$l \le 25 \text{ km}$$

$$\begin{bmatrix} V_S \\ I_S \end{bmatrix} = \begin{bmatrix} 1 & Z \\ 0 & 1 \end{bmatrix} \begin{bmatrix} V_R \\ I_R \end{bmatrix}$$

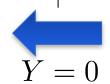


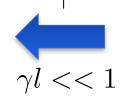
$$l \le 250 \text{ km}$$

$$\begin{bmatrix} V_S \\ I_S \end{bmatrix} = \begin{bmatrix} 1 + \frac{YZ}{2} & Z \\ Y\left(1 + \frac{YZ}{4}\right) & 1 + \frac{YZ}{2} \end{bmatrix} \begin{bmatrix} V_R \\ I_R \end{bmatrix} \quad \begin{bmatrix} V_S \\ I_S \end{bmatrix} = \begin{bmatrix} \cosh(\gamma l) & Z_c \sinh(\gamma l) \\ \frac{1}{Z_c} \sinh(\gamma l) & \cosh(\gamma l) \end{bmatrix} \begin{bmatrix} V_R \\ I_R \end{bmatrix}$$



$$\begin{bmatrix} V_S \\ I_S \end{bmatrix} = \begin{bmatrix} \cosh(\gamma l) & Z_c \sinh(\gamma l) \\ \frac{1}{Z_c} \sinh(\gamma l) & \cosh(\gamma l) \end{bmatrix} \begin{bmatrix} V_R \\ I_R \end{bmatrix}$$







• How much is the surge impedance of a lossless line?

• What happens when we connect at the end of the line a load equal to the surge impedance of the line?



Surge impedance loading

- How much is the surge impedance of a lossless line?
- The surge impedance of a lossless line is pure resistive

$$Z_c = \sqrt{\frac{L}{C}}$$

- At surge impedance loading the power line is in a state of reactive power balance
 - Series inductances consume the same amount of reactive power as the shunt capacitances produce
 - Reactive power consumed on series inductance: dependent on current through the line
 - Reactive power consumed on shunt capacitance: dependent on voltage at line ends

5



Reactive power demand of a line

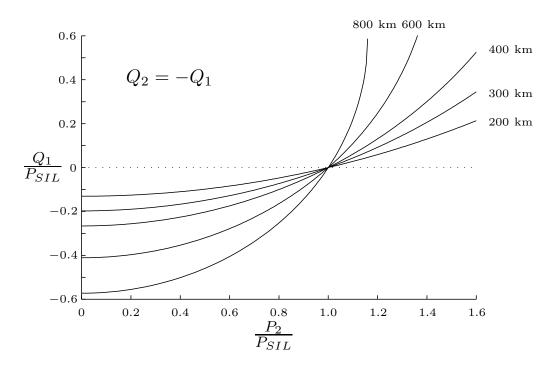


Figure 6.3. The reactive power demand at the beginning of the line, as a function of the active power at the end of the line $(U_1 = U_2, lossless line)$.



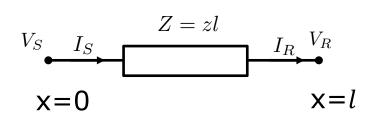
Voltage Profiles

FIGURE 5.10 V(x) + Voltage profiles of $V_{RNL} = V_{S}/\cos(\beta \ell)$ an uncompensated No-losd lossless line with fixed sending-end voltage for line SIL lengths up to a $V_{RSIL} = V_{S}$ Full load quarter wavelength Short circuit VRFL $V_{RSC} = 0$ $x = \ell$ x = 0Sending end Receiving end

Figure taken from: J. Glover, T. Overbye, M. Sarma, Power System Analysis and Design, Cengage Learning, Sixth Edition, 2016

Voltage at the beginning of the line for different power factors





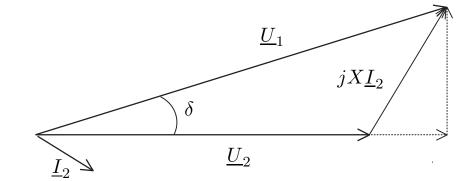


Figure 6.7. Simplified relation between the phasors \underline{U}_1 and \underline{U}_2 .

- The above diagram shows the voltage and current phasors for an inductive load (lagging power factor) and a line modelled as a series inductance
- Draw the phasor diagrams and describe what happens with the voltage angle and magnitude for:
 - 1. $cos\phi = 1$
 - 2. $P=P_{SII}$ (here you must use the exact parameters/equations for the lossless lines)
 - 3. cosφ : leading



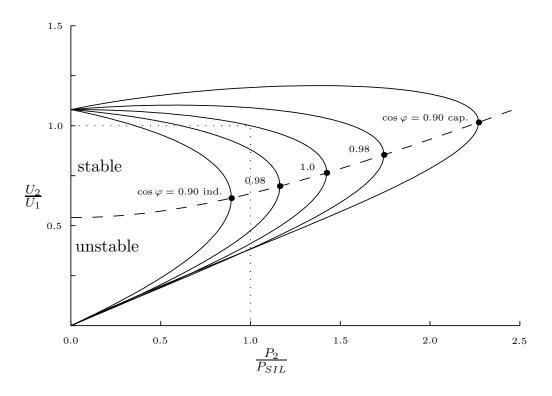


Figure 6.10. Voltage at the end of the line as a function of the delivered active power for different line loadings. U_1 is kept constant at 1.0 pu.



Steady-state stability limit

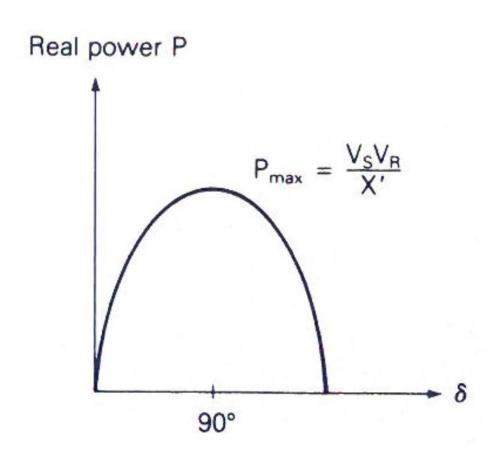


FIGURE 5.11

Real power delivered by a lossless line versus voltage angle across the line



Line Loadability

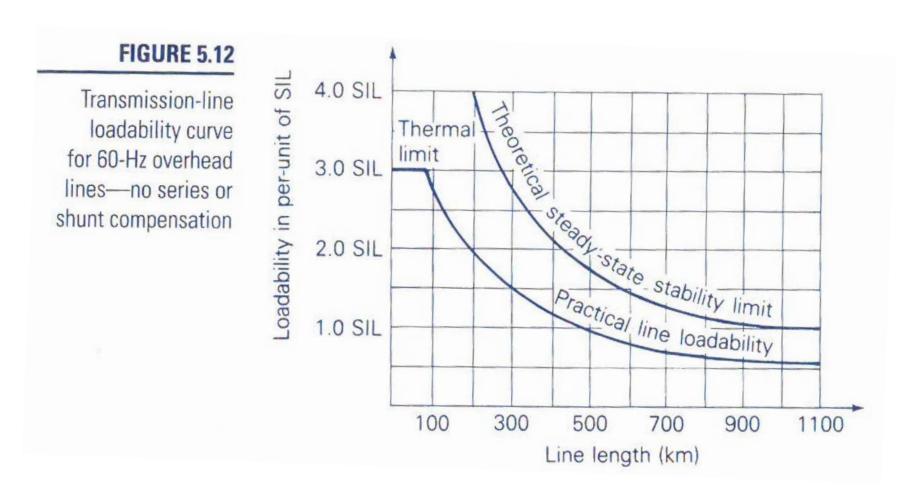


Figure taken from: J. Glover, T. Overbye, M. Sarma, Power System Analysis and Design, Cengage Learning, Sixth Edition, 2016



Shunt Reactive Compensation

- You are given:
 - 1. Nominal voltage at full load conditions
 - 2. Current at full load conditions
- You need to determine
 - Nominal voltage at sending end
 - Percent voltage regulation at no-load conditions
 - Shunt reactive compensation to stay within limits